

# LIGHTNING: EARTHING ELECTRODES HARMONIC RESPONSE

AGUADO M. HERMOSO B. SENOSIAIN V.

MARTÍNEZ-CID P.

Public University of Navarra

Iberdrola

(Spain)

**1.- Abstract.** The grounding behavior (resistive, capacitive, inductive) to a lightning discharge is related to the electrodes geometrical dimensions [1], shapes, and the soil characteristics (resistivity  $\rho$ , permittivity  $\epsilon$ , permeability  $\mu$ ). The border between the capacitive and inductive behaviors corresponds to a frequency value (critical frequency  $f_c$ ), analyzed with the T line model. A practical relation ( $f_c$ ,  $\rho/l$ ) is obtained from variable frequency tests made over different electrodes.

**2.- Introduction.** To analyze the response of a ground electrode when a lightning discharge is scattered, we use the T line model (fig 1):

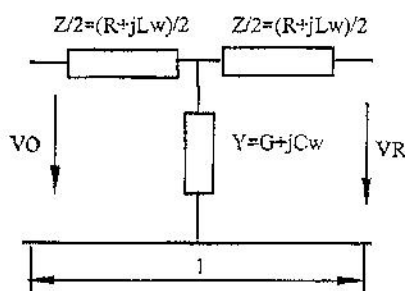


Fig.1. T line model

The expression for the input impedance is:

$$Z = \frac{jL\omega}{2} + \frac{1}{Y} = \frac{jL\omega}{2} + \frac{R_E}{1 + jR_EC\omega} = \frac{jL\omega}{2} + \frac{R_E(1 - jR_EC\omega)}{1 + R_E^2C^2\omega^2} = \frac{R_E}{1 + R_E^2C^2\omega^2} + j\omega \left( \frac{L}{2} - \frac{R_E^2C^2L\omega^2}{1 + R_E^2C^2\omega^2} \right)$$

in which one the complex part value is function of the sing of  $(L/2 - R_E^2C)$ , if:

- $(L/2 - R_E^2C) > 0$  there is an inductive behavior for all frequencies.
- $-(L/2 - R_E^2C) < 0$  there is capacitive behavior for the region between  $\omega = 0$ ,  $\omega = \omega_c$
- $-(L/2 - R_E^2C) = 0$  resistive behavior for all frequencies.

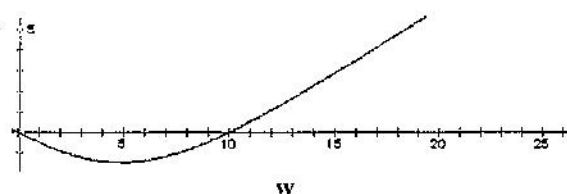


Fig.2 Zi Capacitive-Inductive behavior

For the last case the  $\omega_c$  and  $f_c$  values are:

$$\omega_r = \sqrt{\frac{2R_E^2C - L}{R_E^2C^2L}} \quad f_r = \frac{1}{2\pi} \sqrt{\frac{2R_E^2C - L}{R_E^2C^2L}}$$

**3.- Critical Frequency.** Theoretically, from the  $f_c$  expression, one can choose values for  $R_E$ ,  $L$  and  $C$  in a way that the grounding system works in capacitive zone for lightning discharge (1-2 Mhz.) [4] Taking in account the values of  $R_E$ ,  $L$  and  $C$  are functions of soil characteristics ( $\rho$ ,  $\mu$ ,  $\epsilon$ ) and electrodes shape and dimension, we can write  $f_c = f_c(\rho, \mu, \epsilon, l)$ . To evaluate this expression, not in a theoretically way, we have done field tests. According the fall voltage method (fig.3) we injected an ac current wave in 1 using a frequency multifunction waveform synthesizer *Rohde and Schwarz* with output impedance of  $50 \Omega$  and a coaxial wire RG58U. We measured the voltage  $V$  (figure 4 to 6) in different electrodes and soils with a Fluke99 Scopemeter.

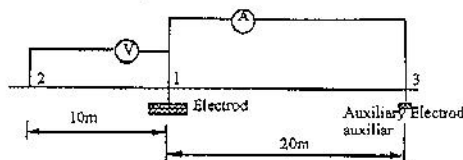


Fig.3. Impedance measurement circuit

We linked the  $f_c$  values to  $\rho/l$  ones, ( $l$  electrode length). In the lasts tests (fig.7) we have recorded the voltage and current

simultaneously. The current ( $A$ ) has been measured by a coupled current probe A6312-DC and a current probe amplifier AM508B.

The three firsts tests are been made up through a project financed by the Spanish Railway Company RENFE, and the last one through another one financed by the Companies EHN, Gamesa Eólica and Iberdrola.

- *Electrode 1:*  $\rho=50 \Omega.m$ ,  $l=1,5m$

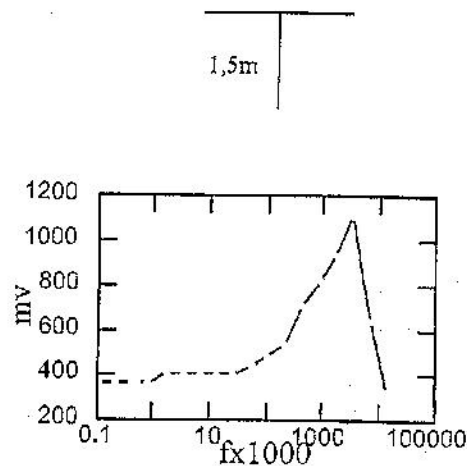
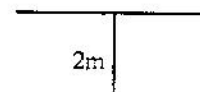


Fig.4. Frequency response electrode 1

$f_c=50kHz$ ,  $\rho/l=33,33$

- *Electrode 2:*  $\rho=50 \Omega.m$ ,  $l=2m$



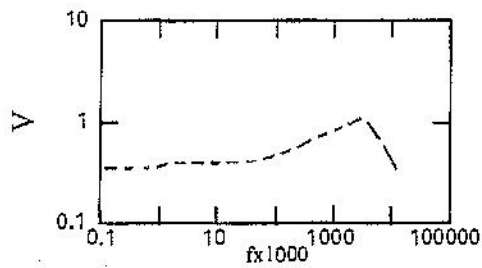


Fig.5. Frequency response electrode 2

$$f_c = 50 \text{ kHz}, \rho/l = 25$$

- Electrode 3:  $\rho = 200 \Omega\text{m}$ ,  $l = 6\text{m}$

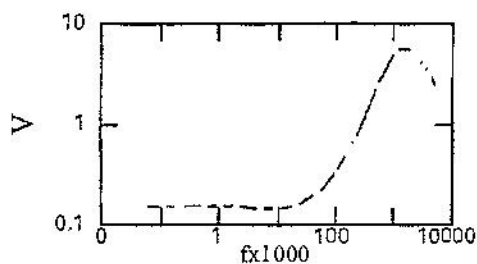
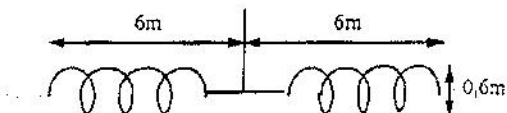


Fig.6. Frequency response electrode 3

$$f_c = 20 \text{ kHz}, \rho/l = 33,33$$

- Electrode 4:  $\rho = 800 \Omega\text{m}$ ,  $l = 1,5\text{m}$

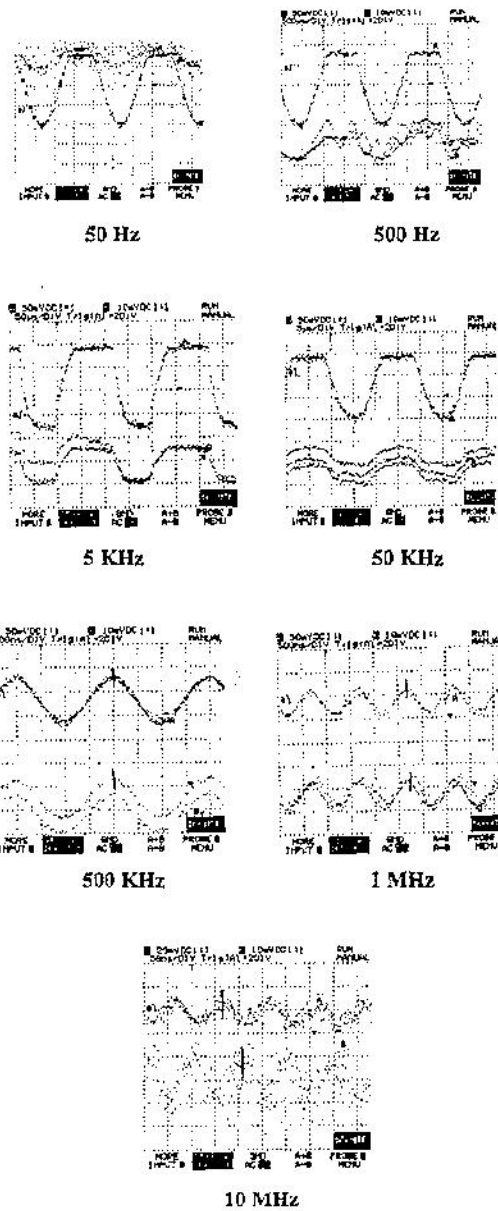
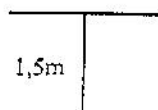


Fig.7. Frequency response electrode 4

One can observe that at 10 MHz the current lag voltage.

$$f_c = 5 \text{ MHz}, \rho/l = 533,33$$

Recording ( $f_c - \rho/l$ ) we obtain fig.8

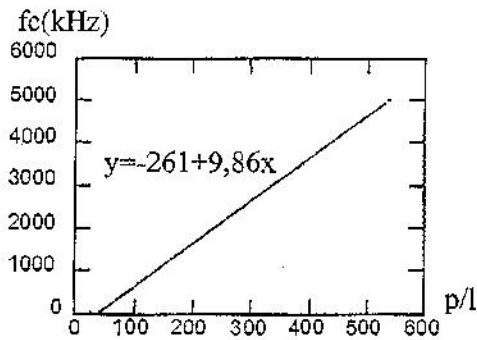


Fig.8. Relationship  $f_c$ - $\rho/l$

for 1-2 MHz the ratio  $\rho/l$  must be between 120-220, and higher for higher frequencies scattered, existing a critical length ( $l_c$ ) for every one  $f_c$ . If  $l$  is longer than  $l_c$  the electrode behavior is inductive.

Example:  $f_c$  1MHz,  $\rho/l = 120$

$\rho$  ( $\Omega \cdot m$ ) 300 500 1000

$l_c$  (m) 2,5 4,17 8,333

figures according with obtained in [3]

#### 4.- Conclusions.

- The border between the capacitive and inductive behavior for a grounding system is related to the critical frequency.
- The critical frequency  $f_c$  is a function of soil characteristics and electrode dimensions ( $\rho$ ,  $\epsilon$ ,  $\mu$ ,  $l$ ).

- There is a relation between  $f_c$  and  $\rho/l$ .

Are necessary more tests (different electrodes shapes and lengths, soils) to consolidate the relation.

- For each  $f_c$  there is an electrode critical length ( $l_c$ ); for  $l > l_c$  the electrode behavior is inductive.

#### 5.- Bibliography

[1] CIGRE 33.01. *Guide to Procedures for Estimating the Lightning Performance of Transmission Lines*. CIGRE, Oct, 91.

[2] Gary C.; *The Earthing Impedance of Horizontally Buried Conductors*. Congress Lightning and Mountains 1994, Chamonix (France)

[3] Bourg S., Sacepe B., Debu T.; *Deep Earth Electrodes in Highly Resistive Ground; Frequency Behavior*. Congress Lightning and Mountains 1997, Chamonix (France).

[4] Aguado M., Hermoso B., Senosiain V., Martínez Cid P.; *Harmonic Impedance of Earthing Electrodes. Lines T Model*. CIGRE; SC 33 International Conference, Zagreb, Croatia, September

1998.

#### **6. Address of Authors**

Dr. Blas Hermoso, D. Vicente Senosian,  
Dña. Mónica Aguado School of Industrial  
Engineering, Electrical Department,  
Public University of Navarra, Campus  
Arrosadia s/n, Pamplona 31008, Navarra,  
Spain

E-mail: [hermoso@upna.es](mailto:hermoso@upna.es),

[vajra@upna.es](mailto:vajra@upna.es), [monica.aguado@upna.es](mailto:monica.aguado@upna.es),

D. P. Martinez Cid, IBERDROLA,  
Gardoqui 8, Bilbao 48008, Spain